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(54) Electronic ignition device with limitation of the voltage at an ignition coil primary winding terminal

(57) The electronic ignition device (50) comprises: an ignition coil (2) having a primary winding terminal (5) and a secondary winding terminal (6) generating a spark; a power element (3) arranged between the primary winding terminal (5) and ground (GND); a protection circuit (11) issuing a disable signal to the control terminal (8) of the power element (3) in preset conditions; and a voltage limiting circuit (51) having inputs (54, 55) connected to the primary winding terminal (5) and to the battery voltage ( $V_B$ ), and an output (56) connected to

the control terminal (8) of the power element (3). The voltage limiting circuit (51) detects a potential difference between its own inputs (54, 55) and supplies to the control terminal (8) an activation signal for the power element (3), in presence of the deactivation signal and when the potential difference exceeds the supply voltage ( $V_B$ ) by a preset value. Thereby, the voltage limiting circuit (51) limits the voltage on the primary winding terminal (5) to a preset value ( $V_L$ ) which depends upon the value of the battery voltage ( $V_B$ ).

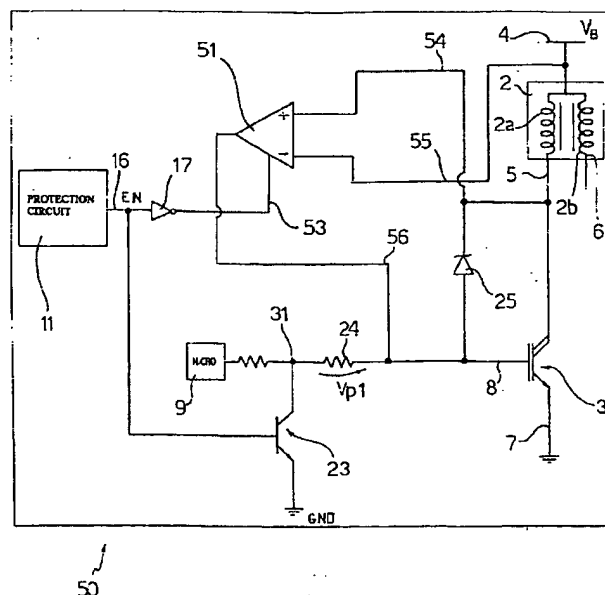


Fig.4

## Description

[0001] The present invention regards an electronic ignition device with limitation of the voltage at an ignition coil primary winding terminal.

[0002] As is known, one of the problems present in electronic ignition devices for inductive loads is to limit the voltage at the primary winding terminal of the ignition coil, in the event of a malfunctioning of the device being detected, so as to prevent an ignition spark from being generated on the secondary winding terminal of the same coil.

[0003] In this connection, Figure 1 shows a schematic circuit diagram of an electronic ignition device 1 comprising an ignition coil 2 and a power element 3, for example an IGBT or a bipolar power transistor. In greater detail, the ignition coil 2 includes a primary winding 2a and a secondary winding 2b; a first terminal 2c of the primary and secondary windings 2a, 2b is connected to a supply line 4, set at a battery voltage  $V_B$ , a second terminal 5 of the primary winding 2a is connected to a collector terminal of the power element 3, and a second terminal 6 of the secondary winding 2b is connected to a spark plug (not shown in Figure 1) which generates the ignition spark. The power element 3 has an emitter terminal 7 connected to ground GND and a control terminal 8 connected to a microprocessor 9, shown only schematically in Figure 1, through a resistor 10. A high voltage Zener diode 25 has its cathode connected to the second terminal 5 of the primary winding 2a and its anode connected to the control terminal 8 of the power element 3. The high voltage Zener diode 25 limits the maximum voltage applied to the second terminal 5 of the primary winding 2a to prevent the latter from exceeding the breakdown voltage of the power device 1.

[0004] The microprocessor 9 controls turning on of the power element 3 by supplying, to the control terminal 8 of the latter, a trigger signal at a high logic level (Figure 2). Upon turning on of the power element 3, across the primary winding 2a a voltage is applied that is close to the battery voltage  $V_B$ . Consequently, a primary current  $I_{out}$  starts flowing in the terminal of the primary winding 5 (Figure 2).

[0005] Once an appropriate time has elapsed during which the primary current  $I_{out}$  reaches a preset value  $I_0$  (charging time of the ignition coil 2), the microprocessor 9 controls turning off of the power device 3 by sending the trigger signal to a low logic level. In this condition, a voltage pulse  $V_0$  is generated at the second terminal 5 of the primary winding 2a (Figure 2); the voltage pulse, transferred onto the second terminal of the secondary winding 2b multiplied by the turn ratio of the ignition coil 2, gives rise to a spark.

[0006] In an electronic ignition device of the type described above, it is necessary that the spark is generated only when the microprocessor 9 turns off the power element 3 by sending the trigger signal to the low logic level. However, in the event of malfunctioning of the de-

vice, it may be necessary to turn off the power element 3 independently of the logic level of the trigger signal and without a spark being produced on the second terminal 6 of the secondary winding 2b.

[0007] As shown in Figure 3, to meet this requirement, the electronic ignition device 1 is provided with a protection circuit 11, shown only schematically in Figure 3, for detecting anomalous operating conditions of the electronic ignition device 1, such as overheating of the power element 3 or exceeding the preset current value  $I_0$ , and supplying, at an output terminal 16, a logic signal EN used as enable signal for a voltage limiting circuit 12.

[0008] In greater detail, the voltage limiting circuit 12 has a first input terminal 13, a second input terminal 14, and an output terminal 15. The first input terminal 13 of the voltage limiting circuit 12 is connected to the second terminal 5 of the primary winding 2a; the second input terminal 14 of the voltage limiting circuit 12 is connected to the output terminal 16 of the protection circuit 11 through an inverter 17; and the output terminal 15 of the voltage limiting circuit 12 is connected to the control terminal 8 of the power element 3.

[0009] The voltage limiting circuit 12 comprises an enable transistor 18 of the NPN type, having a collector terminal connected to the first input terminal 13 of the voltage limiting circuit 12 through a high voltage resistor 19, an emitter terminal connected to ground GND, and a control terminal connected to the second input terminal 14 of the voltage limiting circuit 12.

[0010] The voltage limiting circuit 12 further comprises a first high voltage vertical transistor 20a and a second high voltage vertical transistor 20b, both of the NPN type and coupled in Darlington configuration. In particular, the first high voltage vertical transistor 20a has a collector terminal connected to the first input terminal 13 of the voltage limiting circuit 12, a control terminal connected to the collector terminal of the enable transistor 18 through a first circuit node 30, and an emitter terminal. The second high voltage vertical transistor 20b has a collector terminal connected to the first input terminal 13 of the voltage limiting circuit 12, a control terminal connected to the emitter terminal of the first transistor 20a, and an emitter terminal connected to the output terminal 15 of the voltage limiting circuit 12 through a Zener diode 22. The Zener diode 22 has its cathode connected to the emitter terminal of the second transistor 20b and its anode connected to the output terminal 15 of the voltage limiting circuit 12. A resistive element 21 is connected between the control terminal and the emitter terminal of the second high voltage vertical transistor 20b.

[0011] The electronic ignition device 1 further comprises a protection transistor 23 having a collector terminal connected to the control terminal 8 of the power element 3 via a second circuit node 31, an emitter terminal connected to ground GND, and a control terminal connected to the output terminal 16 of the protection circuit 11.

[0012] A biasing resistor 24 coupled between the sec-

ond circuit node 31 and the output terminal 15 of the voltage limiting circuit 12.

[0013] After detecting a malfunctioning of the electronic ignition device 1, the protection circuit 11 generates, on the control terminal of the protection transistor 23, a high logic level of the logic signal EN. Consequently, the protection transistor 23 saturates, generating on the second circuit node 31 a voltage  $V_{cesat}$  equal to its own saturation voltage (voltage present between the collector and the emitter terminal of the protection transistor 23 in saturation) and determining turning off of the power element 3, with consequent increase in the voltage on the second terminal 5 of the primary winding 2a.

[0014] At the same time, the inverter 17 generates, on the control terminal of the enable transistor 18, a logic signal, correlated to the logic signal EN, at a low logic level. Consequently, the enable transistor 18 turns off, generating on the first circuit node 30 a voltage that turns on the high voltage vertical transistors 20a and 2b. These transistors supply the Zener diode 22 and the biasing resistor 24 with a current that causes a biasing voltage  $V_P$  across the biasing resistor 24. The biasing voltage  $V_P$  causes turning on again of the power element 3, which maintains the voltage on the second terminal 5 of the primary winding 2a at a value  $V_L$  that maintain the high voltage vertical transistors 20a, 20b on, so that the latter continue to supply current until complete exhaustion of the energy stored in the primary winding 2a of the ignition coil 2. In particular, the value  $V_L$  is

$$V_L = V_R + V_{be1} + V_{be2} + V_Z + V_P + V_{cesat} \quad (1)$$

wherein  $V_R$  is the voltage across the high voltage resistor 19,  $V_{be1}$  and  $V_{be2}$  are the voltages between the control and the emitter terminals of the high voltage vertical transistors 20a, 20b, and  $V_Z$  is the voltage across the Zener diode 22.

[0015] At the end of the discharge of the ignition coil, the voltage  $V_L$  reaches the value of battery voltage  $V_B$ . In these conditions, for proper operation of the voltage limiting circuit 12, the high voltage vertical transistors 20a, 20b must be off. This occurs only if the voltage  $V_Z$  satisfies the following condition:

$$V_Z > V_B - V_R - V_{be1} - V_{be2} - V_P - V_{cesat} \quad (2)$$

which is obtained from relation (1) setting  $V_L = V_B$ .

[0016] Consequently, on the basis of relation (2), in order to have proper operation of the voltage limiting circuit 12, the Zener diode 22 must be chosen each time according to the maximum battery voltage  $V_B$  envisaged in the specifications.

[0017] In addition, in applications for electronic ignition that require a preset maximum value of 24 V for the battery voltage  $V_B$ , the value of the voltage  $V_L$  may be

to high if the coil has a high turn ratio between its primary and its secondary windings; consequently, an undesired spark may be generated.

[0018] The technical problem to be solved by the present invention is to provide an electronic ignition device limiting the voltage existing at the primary winding terminal of the ignition coil, which may overcome prior art limitations and drawbacks.

[0019] This problem is solved by an electronic ignition device as defined in Claim 1.

[0020] The features and advantages of the electronic ignition device according to the invention will emerge clearly from the following description of an embodiment, given only as a non-limiting example, with reference to the attached drawings, wherein:

- Figure 1 is a schematic circuit diagram of a known electronic ignition device;
- Figure 2 shows the plots of electrical quantities taken on the device of Figure 1;
- Figure 3 presents a more complete circuit diagram of the electronic ignition device of Figure 1;
- Figure 4 shows a circuit diagram of an electronic ignition device according to the invention;
- Figure 5 shows a more detailed circuit diagram of an electronic ignition device according to the invention; and
- Figure 6 shows a cross-section through a chip incorporating a portion of the electronic ignition device of Figure 4.

[0021] Figure 4 shows the circuit diagram of an electronic ignition device 50 according to the invention, comprising a voltage limiting circuit comprising an operational amplifier 51.

[0022] The operational amplifier 51 has an enable terminal 53 connected, through the inverter 17, to the output terminal 16 of the protection circuit 11, a non-inverting terminal 54, connected to the second terminal 5 of the primary winding 2a, an inverting terminal 55 connected to the supply line-4, and an output terminal 56 connected to the control terminal 8 of the power element 3.

[0023] The other parts of the electronic ignition device 50 are equal to those of the known electronic ignition device 1 shown in Figures 1 and 3; consequently, they are designated by the same reference numbers and will not be described any further.

[0024] In greater detail, as shown in Figure 5, the operational amplifier 51 comprises an NPN type, enable transistor 57 having a collector terminal connected to the non-inverting terminal 54 through a high voltage resistor 58, an emitter terminal connected to ground GND, and a control terminal connected to the enable terminal 53.

[0025] The operational amplifier 51 further comprises an NPN type high voltage vertical transistor 59 having a collector terminal connected to the non-inverting ter-

terminal 54, a control terminal connected, at a first circuit node 60, to the collector terminal of the enable transistor 57, and an emitter terminal.

[0026] A PNP type error transistor 61 defining an error amplifier has an emitter terminal connected to the emitter terminal of the high voltage vertical transistor 59, a control terminal connected to the inverting terminal 55, and a collector terminal connected to the output terminal 56 through a current amplifier block 62, illustrated only schematically in Figure 4 and per se known.

[0027] The current amplifier block 62 has a supply terminal 63 connected to the inverting terminal 55.

[0028] As shown in Figure 6, the voltage limiting circuit 51 is implemented using a VIPOWER™ technology, which enables integrating, in a same chip 100, a high voltage circuit portion 101 of the voltage limiting circuit 51 and a low voltage circuit portion 102 of the voltage limiting circuit 51, which are separated from each other by an isolation region 103 having P-type conductivity. In greater detail, the high voltage circuit portion 101 accommodates the high voltage vertical transistor 59 and the high voltage resistor 58, the latter being made as a prolongation of a base region 104 belonging to the high voltage vertical transistor 59. The low voltage circuit portion 102 accommodates the enable transistor 57 and the error transistor 61 as well as the current amplifier block 62 (not shown in Figure 6).

[0029] Operation of the electronic ignition device 50 of Figure 4 is described hereinbelow.

[0030] Similarly to the above, the protection circuit 11, after detecting a malfunctioning of the electronic ignition device 50, generates, at the output terminal 16 of the protection circuit 11, a high logic level of the logic signal EN, thus turning off the power element 3 and enabling the operational amplifier 51.

[0031] Once enabled, the operational amplifier 51 operates so as to maintain its own input terminals 54, 55 at the same potential and supplies on its own output terminal 56 a current which determines, across the biasing resistor 24, a biasing voltage  $V_{P1}$  which causes the power element 3 to turn on again; the latter, in turn, limits the voltage on the second terminal 5 of the primary winding 2a, as well as the voltage present on the non-inverting terminal of the operational amplifier 51, to a value equal to that of the battery voltage  $V_B$ .

[0032] In greater detail, the inverter 17 generates, on the control terminal of the enable transistor 57, a logic signal, correlated to the logic signal EN, at a low logic level. Consequently, the enable transistor 57 turns off, thus enabling the current through the high voltage resistor 58 to flow in the control terminal of the high voltage vertical transistor 58, so turning it on. The current supplied by the high voltage vertical transistor 59 flows in the error transistor 61 and, after being amplified by the current amplifier block 62, is injected into the biasing resistor 24, so generating the biasing voltage  $V_{P1}$ , which, as mentioned, turns on again the power element 3 and limits the voltage on the non-inverting terminal of the op-

erational amplifier 51. In practice, a negative feedback is created, whereby the voltage on the second terminal 5 of the primary winding 2a is limited to a value  $V_{L1}$  according to the following equation:

$$V_{L1} = V_R + V_{be1} + V_{eb2} + V_B \quad (3)$$

where  $V_R$  is the voltage present across the high voltage resistor 58,  $V_{be1}$  is the emitter-to-control terminal voltage of the high voltage vertical transistor 59,  $V_{eb2}$  is the emitter-to-control terminal voltage of the error transistor 61, and  $V_B$  is the battery voltage.

[0033] From the above, it is clear that the electronic ignition device 50 is a negative feedback device in which the error transistor 61 detects, between its emitter and control terminals, the voltage difference existing between the second terminal 5 of the primary winding 2a and the supply line 4 (battery voltage  $V_B$ ), and supplies, on its own collector terminal, a current controlling the power element 3 so that the voltage at the second terminal 5 of the primary winding 2a is not be able to exceed  $V_{L1}$ , according to relation (3).

[0034] The current amplifier block 62 has the purpose of reducing to the utmost the current flowing in the collector terminals of the high voltage vertical transistor 59 and of the error transistor 61 so as to enable the use of components having minimal dimensions; in addition, it minimizes the current flowing in the control terminal of the high voltage vertical transistor 59 and, consequently, the voltage  $V_{R1}$  across the high voltage resistor 58.

[0035] Furthermore, the action of the current amplifier block 62 is particularly important when the power element 3 is a bipolar power transistor, which requires, on its control terminal, an adequate current for turning on again during limitation.

[0036] In normal operating conditions of the electronic ignition device 50, the protection circuit 11 maintains the logic signal EN at a low logic level. The protection transistor 23 is therefore off, whereas the activation transistor 57, in so far as it has a logic signal at a high logic level on its control terminal, is saturated and turns off the high voltage vertical transistor 59. In this way, the error transistor 61 does not supply any current to the biasing resistor 24, and the electronic ignition device 50 can operate regularly, as described above.

[0037] The electronic ignition device 50 described herein has the following advantages. First, unlike the known voltage limiting circuit, wherein it is necessary to use each time a Zener diode 22 correlated to the maximum value selected for the battery voltage  $V_B$ , the present voltage limiting circuit 51 is able to adapt automatically to the maximum value of the battery voltage  $V_B$ , without any need for modifying the circuit.

[0038] In fact, the voltage limiting circuit 51 is always able to limit the voltage present on the second terminal 5 of the primary winding 2a to a voltage value  $V_{L1}$ , irre-

spective of the value of the battery voltage  $V_B$ . The value of the voltage  $V_{L1}$  is also such as to prevent a spark forming on the second terminal 6 of the secondary winding 2b of the ignition coil.

[0039] Furthermore, the voltage limiting circuit 51 comprises a single high voltage transistor 59; in addition, it has smaller dimensions than the high voltage vertical transistor included in the known voltage limiting circuit. Thereby, the size of the voltage limiting circuit 51 according to the invention is considerably reduced.

[0040] Finally, it is clear that numerous variations and modifications may be made to the electronic ignition device described and illustrated herein, all falling within the scope of the invention, as defined in the attached claims. In particular, it is emphasized that the specific implementation shown in Figure 5 is merely presented as an example.

#### Claims

##### 1. An electronic ignition device comprising:

- an ignition coil (2) having a supply terminal (2c) connected to a supply line (4) set at a supply voltage ( $V_B$ ), a primary winding terminal (5), and a secondary winding terminal (6) generating a spark;
- a power element (3) having a first and a second conduction terminals connected, respectively, to said primary winding terminal (5) and to a reference node (GND), and a control terminal (8);
- a disabling circuit (11) having an output terminal (16) coupled to said control terminal (8) of said power element (3), said disabling circuit (11) generating, on said control terminal (8), a disabling signal for said power element (3);
- a voltage limiting circuit (51) having an enable terminal (53) connected to said output terminal (16) of said protection circuit (11), a first input terminal (54) connected to said primary winding terminal (5), and an output terminal (56) connected to said control terminal (8);

characterized in that said voltage limiting circuit (51) has a second input terminal (55) connected to said supply line (4), said voltage limiting circuit (51) detecting a potential difference present between said first input terminal (54) and said second input terminal (55), and generating on said control terminal (8) an activation signal for said power element (3) in presence of said disabling signal and of a preset relation between said potential difference and said supply voltage ( $V_B$ ).

##### 2. The electronic ignition device according to Claim 1, characterized in that said voltage limiting circuit (51) generates said activation signal when said potential

difference exceeds said supply voltage ( $V_B$ ) by a preset value.

##### 3. The electronic ignition device according to Claim 1 or 2, characterized in that said voltage limiting circuit (51) comprises an operational amplifier having an inverting input (55) connected to said supply line (4), a non-inverting input (54) connected to said primary winding terminal (5), and an output terminal (56) connected to said control terminal (8) of said power element (3).

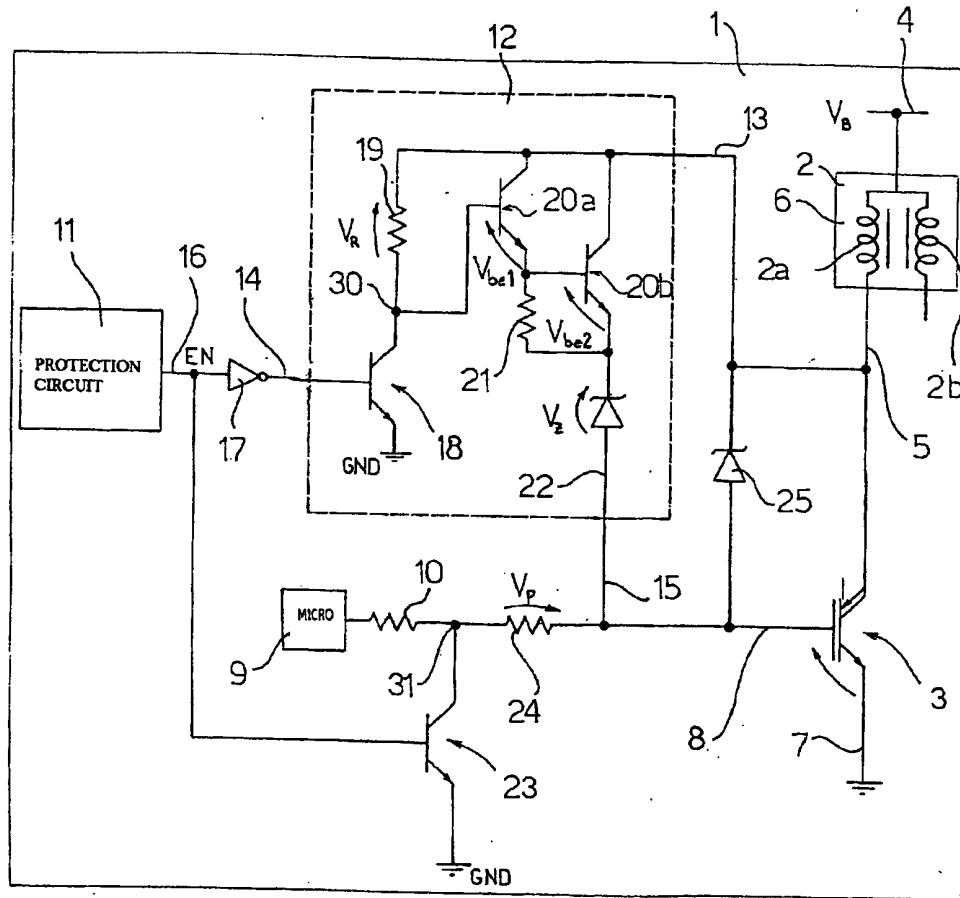
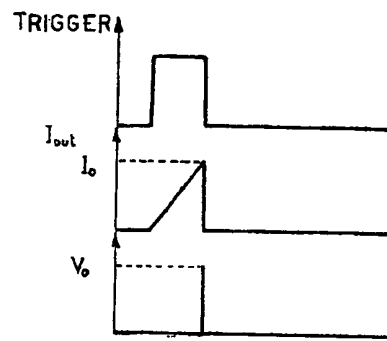
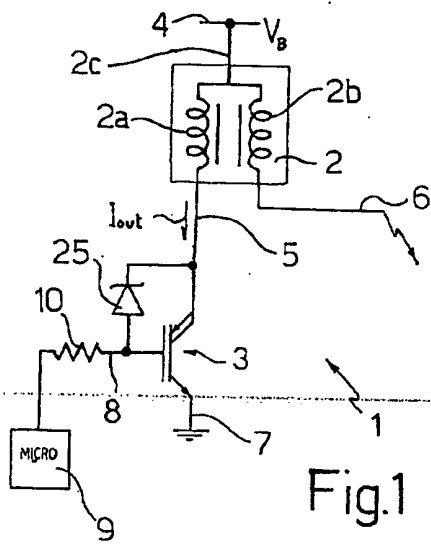
##### 4. The electronic ignition device according to Claim 2 or 3, characterized in that said operational amplifier (51) comprises a first and a second transistor (59, 61) connected in series between said first input terminal (54) and said output terminal (56) of said voltage limiting circuit (51), said first transistor (59) having a control terminal coupled to said enable terminal (53), and said second transistor (61) having a control terminal connected to said second input terminal (55).

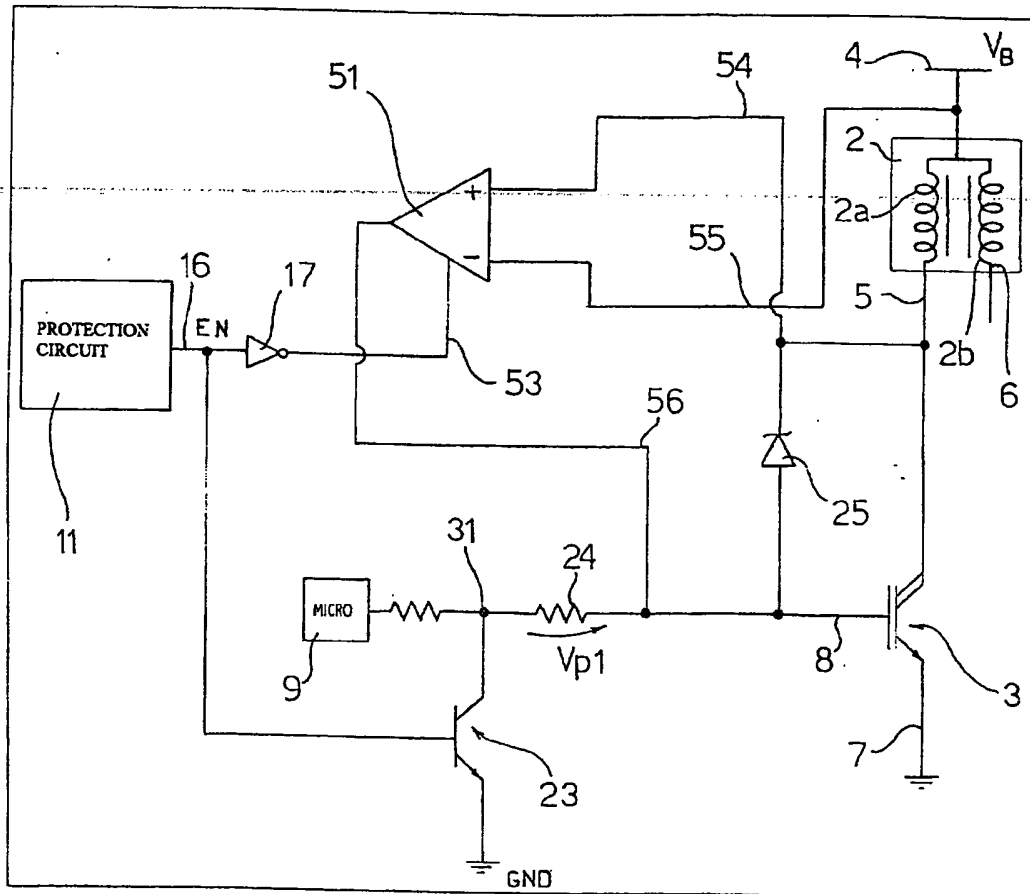
##### 5. The electronic ignition device according to Claim 4, characterized by a current amplifier block (62) arranged between a conduction terminal of said second transistor (61) and said output terminal (56) of said voltage limiting circuit (51).

##### 6. The electronic ignition device according to Claim 4 or 5, characterized in that said control terminal of said first transistor (59) is coupled to said output terminal (16) of said protection circuit (11) through a third transistor (57), said third transistor (57) having a first conduction terminal connected to said control terminal of said first transistor (59), a second conduction terminal connected to said ground terminal (GND), and a control terminal connected to said output terminal (16) of said protection circuit (11).

##### 7. The electronic ignition device according to Claim 6, characterized in that said first transistor (59) is a high voltage vertical transistor of NPN type, said second transistor (61) is of PNP type, and said third transistor (57) is of NPN type.

##### 8. The electronic ignition device according to Claim 6 or 7, characterized in that said first transistor, second and third transistors (59, 61, 57) are integrated in a same chip (100) of semiconductor material.





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Fig.4

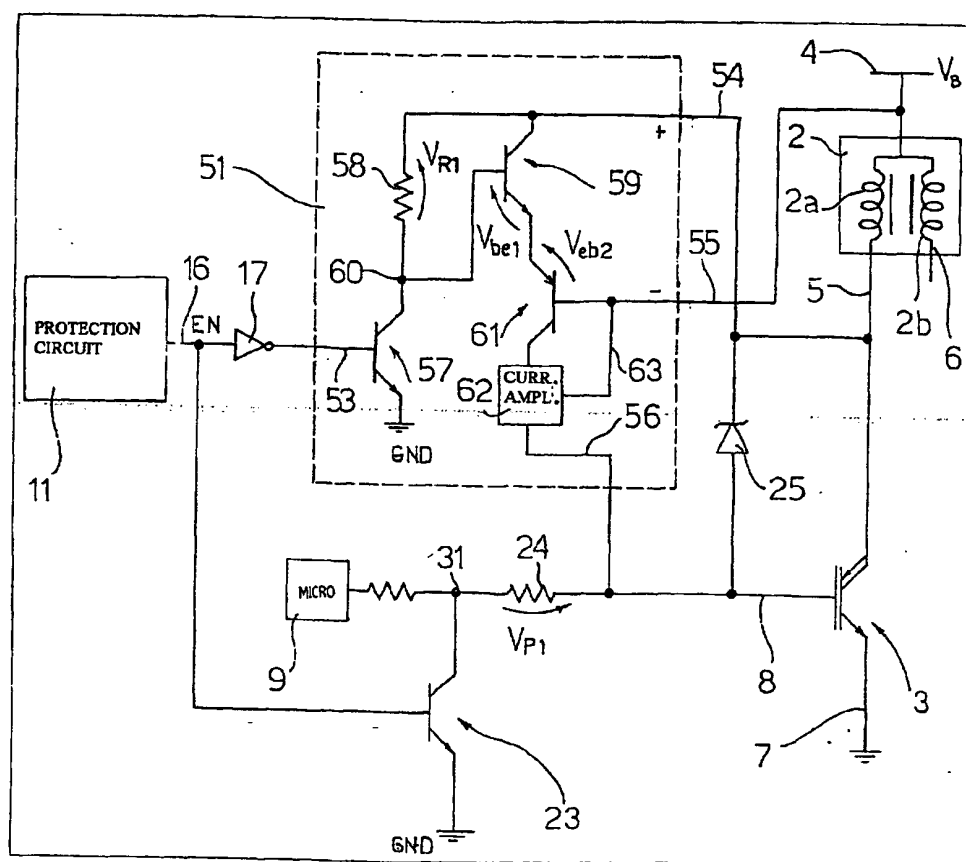


Fig.5

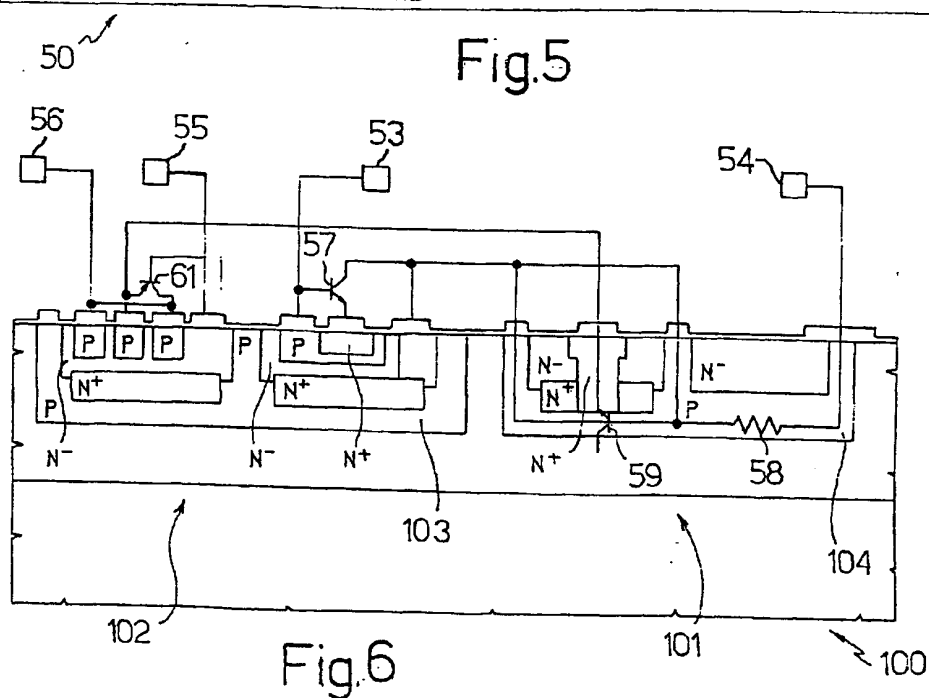


Fig.6





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EP 00 83 0051

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Place of search THE HAGUE		Date of completion of the search 16 June 2000	Examiner Lapeyronnie, P
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